

Limiting Noise

$$i_t = i_s + i_{bg} + i_d$$
$$\sigma_t = (\sigma_s^2 + \sigma_{bg}^2 + \sigma_d^2)^{1/2}$$

Emission and Luminescence:

- $\sigma_t \approx \sigma_{bk}$: Blank noise limited

$\left\{ \begin{array}{l} \sigma_{bk} \gg \sigma_{dt} \text{ (Background noise limited)} \\ \sigma_{bk} \approx \sigma_{dt} \text{ (Dark total noise limited)} \end{array} \right.$

- $\sigma_t \gg \sigma_{bk}$: Analytical Signal noise limited

$\left\{ \begin{array}{l} \sigma_s \propto (i)^{1/2} \text{ (Signal shot noise limited)} \\ \sigma_s \propto i \text{ (Signal flicker noise limited)} \end{array} \right.$

Transmittance:

if $\sigma_s \propto (T)^{1/2}$

if $\sigma_f \propto T$

if $\sigma_{ot} \propto \text{const}$

Analyte concn $\uparrow \rightarrow T \downarrow \downarrow \rightarrow \sigma_{ot}$ limited

Analyte concn $\downarrow \rightarrow T \uparrow \uparrow \rightarrow \sigma_s$ or σ_f limited

$$i_{st} = i_s + i_{ot}$$

12 Spect. In Mod 971204 Sat

S/N ratio enhancement

Emission and/or fluorescence:

Source intensity \uparrow \rightarrow fluoresc. \uparrow

$$I_{tot} = I_F + I_{bg} + I_{dark}$$

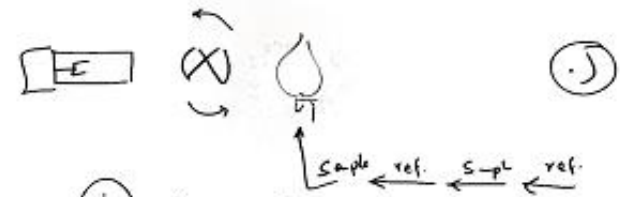
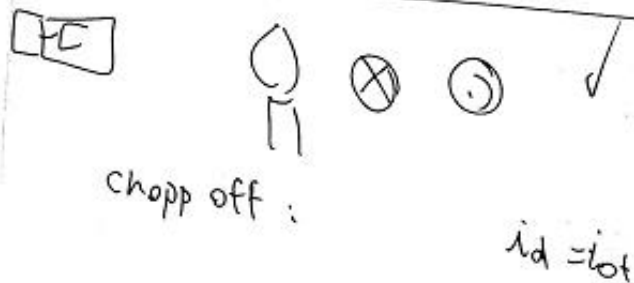
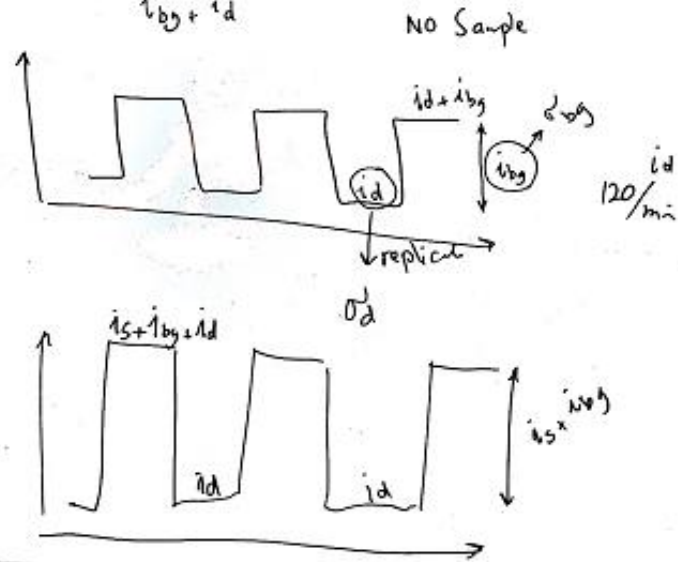
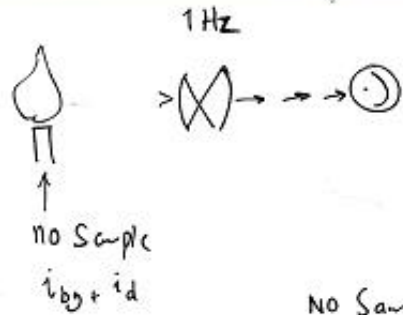
$\underbrace{I_{bg} + I_{dark}}_{I_{bn}}$

Absorbance:

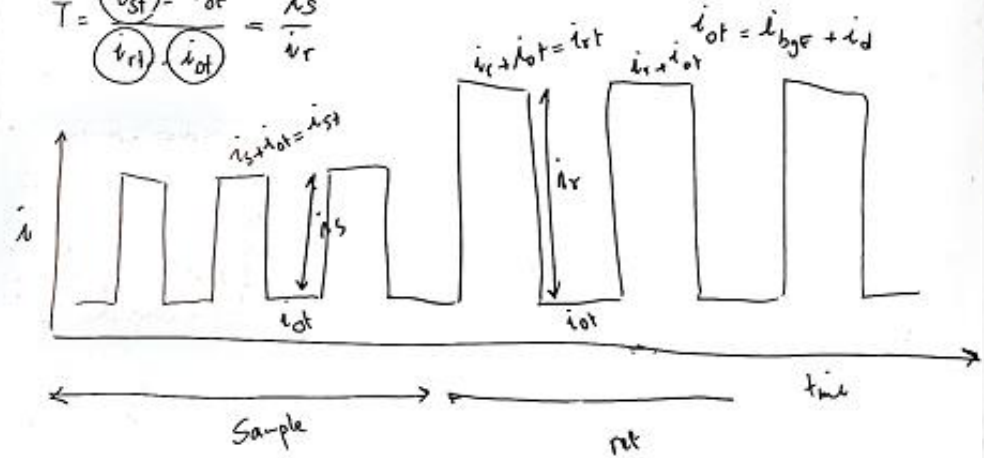
$$T = \frac{E_{st} - E_{ot}}{E_{rt} - E_{ot}}$$

$$A = -\log T$$

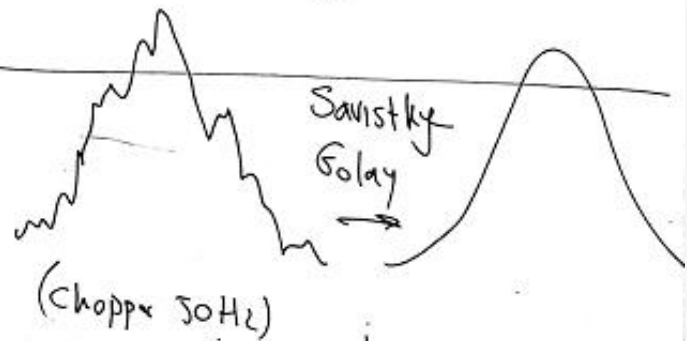
$$I_{st} = I_s + I_{ot}$$



$$T = \frac{I_{st} - I_{ot}}{I_{rt} - I_{ot}} = \frac{I_s}{I_r}$$



Smoothing:



modulation \rightarrow 100 Hz signal \rightarrow filter

5-6 S/N ratio enhancement techniques:

I.

AC or DC signal + Integration and **smoothing** → S/N↑
AC signal + band pass **filter** and lock in amplifier →

II.

$i_B \downarrow \rightarrow S/B \uparrow \rightarrow S/N \uparrow$

III. Photon counting:

Emission and Luminescence:

$$S/N = n_s / \{n_s + n_B + n_d + (\xi n_s)^2 + (\chi n_B)^2\}^{1/2}$$

Amplifier readout and excess dark are not included

Absorbance:

$$\frac{\sigma_A}{A} = (n_r \ln T)^{-1} \left[n_r T^{-1} + (n_r \xi_s)^2 + \frac{n_{bE}}{T^2} + \left(\frac{n_{bEX}}{T} \right)^2 + \frac{n_d}{T^2} \right]^{1/2}$$

Photon counting (digital) condition is preferred to Analog.

Additional noise:

(Independent of analyte signal)

- Detector Noise
- Amplifier readout noise
- Background Noise.

Multiplicative Noise

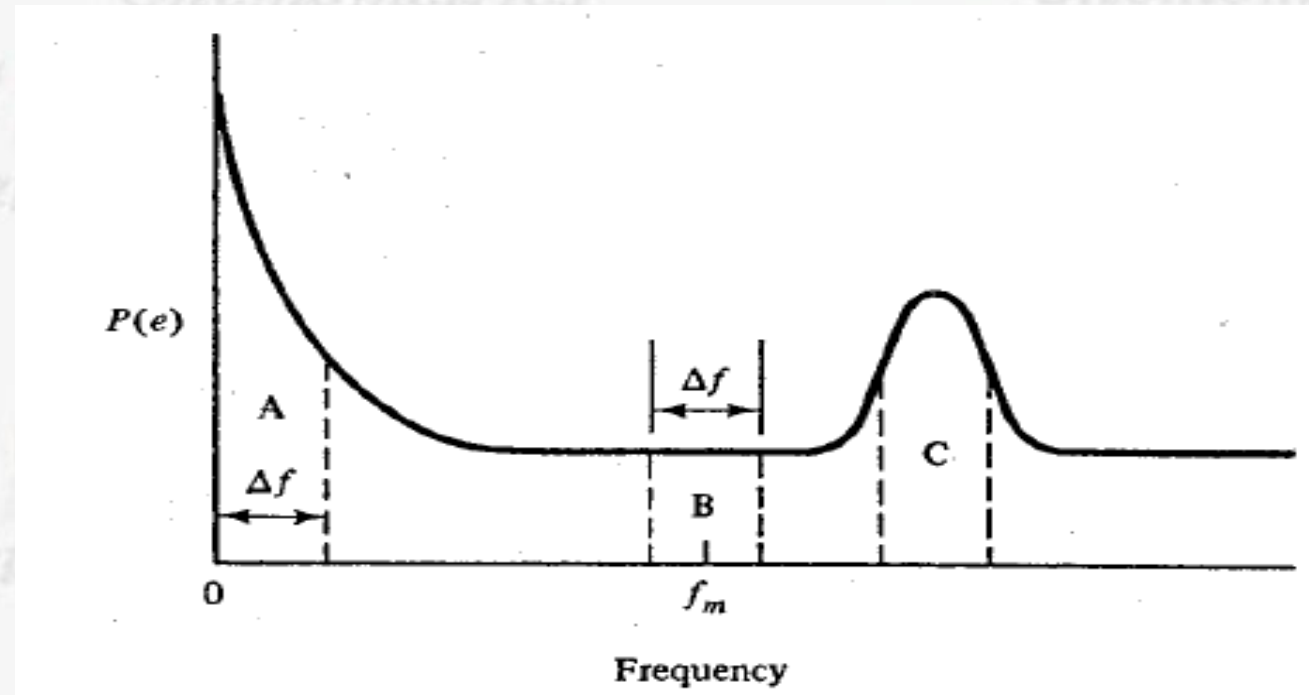
(Dependent on analyte signal)

- Analyte signal shot noise $\propto (i)^{1/2}$
- Analyte signal flicker noise $\propto i$

IV. Modulation:

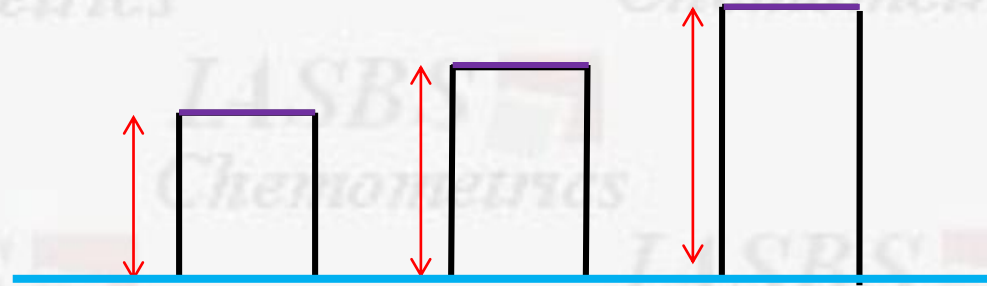
Modulation can be used to change the frequency, (noise power spectrum)

Modulation encodes the signal information at the modulation frequency (f_m),
region (B).



IV. Modulation:

Carried Signal and noise:
Only during one cycle
Ex: Multiplicative
Ex: Additive



Not carried

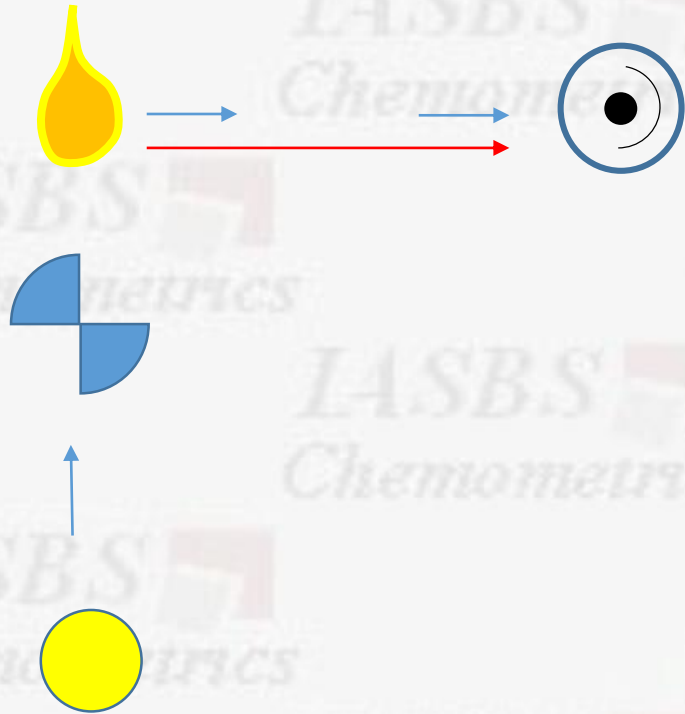
During on and off cycles
Ex: Additive: Background signal and noise

Modulation \rightarrow $S/N \uparrow$
If additive noise: not carried.
Ex: Emission Spectroscopy
+ Sample modul
 \rightarrow Not carried background



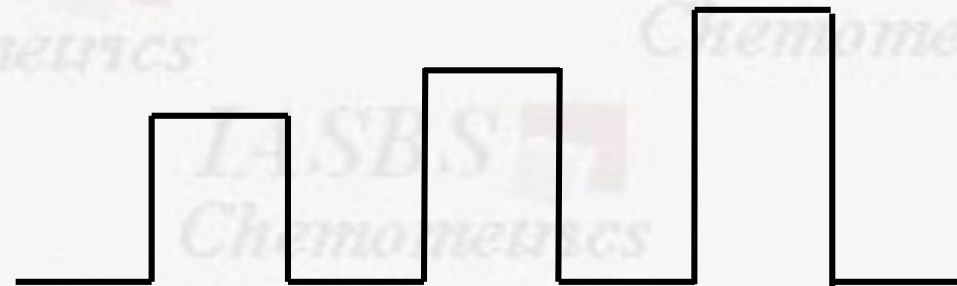
If additive or multiplicative noise is carried S/N does not improve
Ex: Em Spectr + source modulation
 \rightarrow carried backgr emission signal
 \rightarrow no S/N improvement

Atomic Fluorescence + source modulation



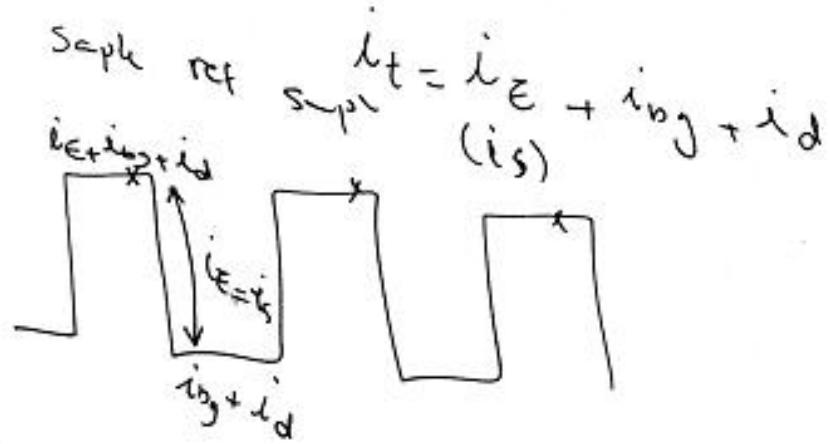
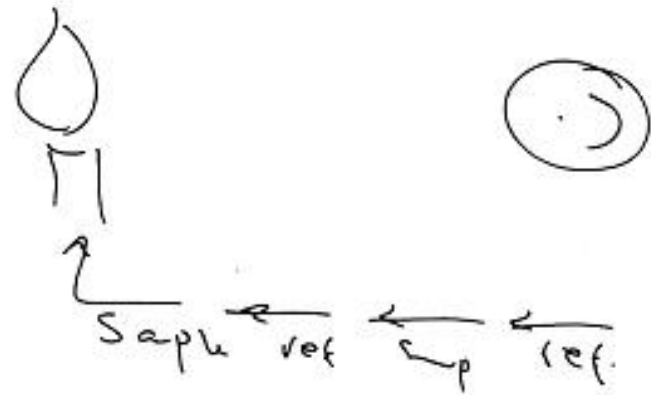
DC source + chopper
Laser + Q-switch
(peak power = 100x DC power)

- Analyte emission: Not carried.
- Backgr Emiss: **Not Carried**
- 1/f of source: Carried
- 1/f of flame: Not Carried
- Analyte luminesce: Carried
- Backgr luminesce: Carried
- Scattering: Carried



+ demodulation

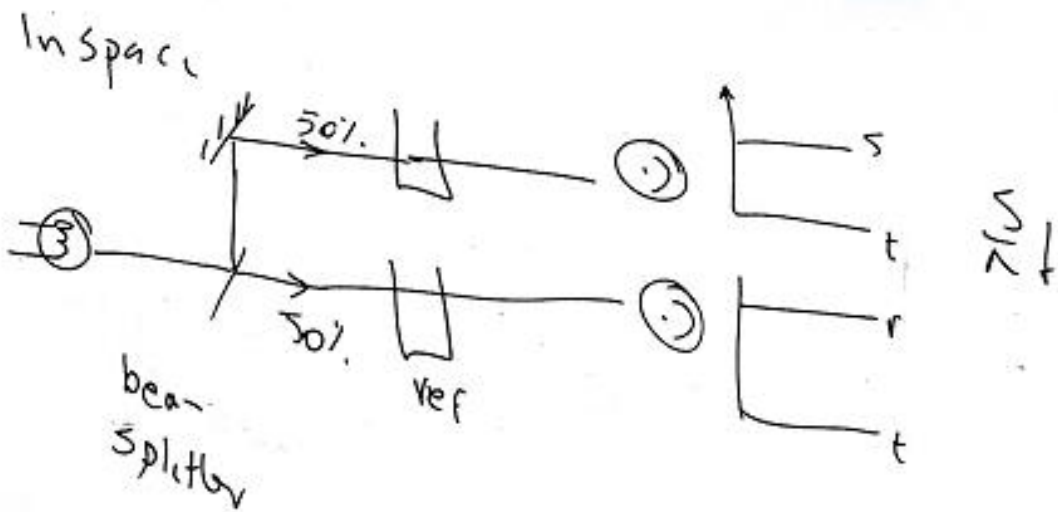
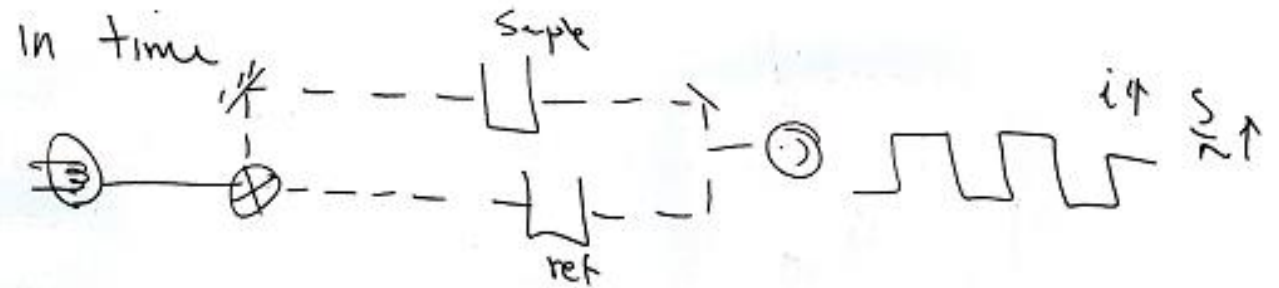
I2 Spect. In Mod 971204 Sat



Non-carried: $I_d + I_o$ (DC)
 Carried: I_e (AC)

Double beam:

Same condition for ref and sample.

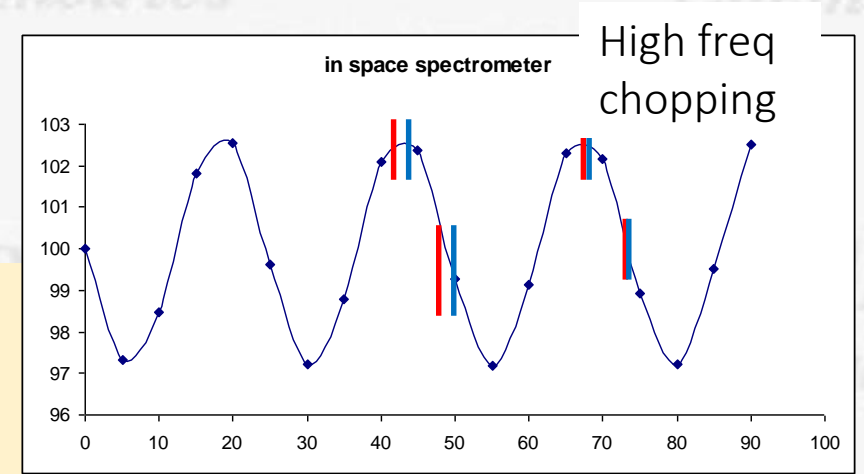


V. Double beam spectrometer.

- In time (chopping);

Should be: freq chopper \gg flicker noise

→ Elimination of $1/f$ and interference noise (if frequency $<$ chopper freq)
of flicker noise (if frequency $<$ chopper freq)



Reference
Sample

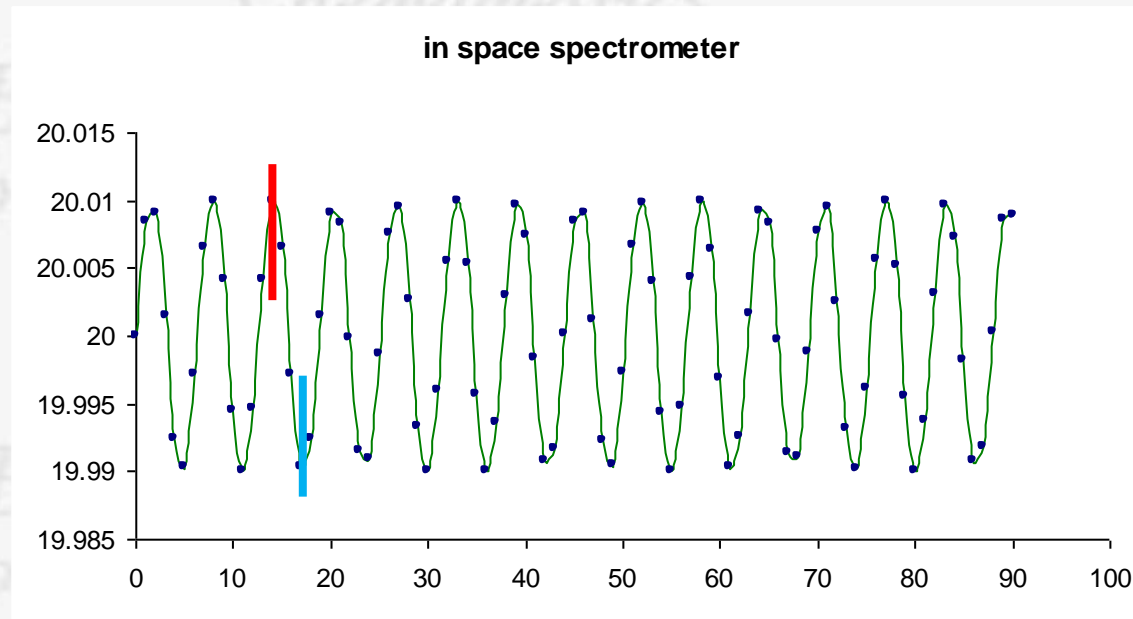
- In Space (dual channel):

→ Elimination of $1/f$ and interference noise (any frequency)
of flicker noise (any frequency)

But: $i_s \downarrow \rightarrow S/N \downarrow$

Ex:
is it possible to
eliminate an
interference noise of
50Hz using a chopping
with 30Hz?

4-2) In space; freq flicker >> freq chapper



VI. Time domain filtering:

Boxcar integrator (in assigned time interval and periode)

if $S/N \propto (n)^{1/2}$

then: integration improves S/N

(reduces the shot noise effect)

Drift should not be exist during integration

(high frequency of signal acquisition),.

Number of scan of electrode charges in photodiode array in a assigned periode of time, is a meaning of integration.

Digital filtering: Fourier transform (time domain, frequency domain)

Smoothing (Savitsky-Golay) $\rightarrow \Delta f \downarrow$

(Moving window, Weighted average)

VII. Multichannel and Multiplexing



15 wavelengths by 15 channels



15 wavelengths by 1 channels

Multichannel and single channel:

Same spectrum in fixed time t for both

→ # photons observed per spectral resolution element is n times greater for multichannel detector.

→ $(S/N)_{\text{MultiCh}} = n^{1/2} (S/N)_{\text{SingCh}}$
(if shot n. limited)

(n : number of spectral resolution elements)

Multiplex systems:

(if shot noise limited)

Michaelson interferometer

n time measuring interferogram
+ FT → n spectra in time t

→ $(S/N)_m = m^{1/2} (S/N)_1$

VIII. High throughput

- Michelson interferometer.
- Dispersion to lower solid angle, and high slit width.
 - high responsivity of detector (not m)
 - lower detector noise



Interference;

- Blank interference,
- Analyte interference

interference

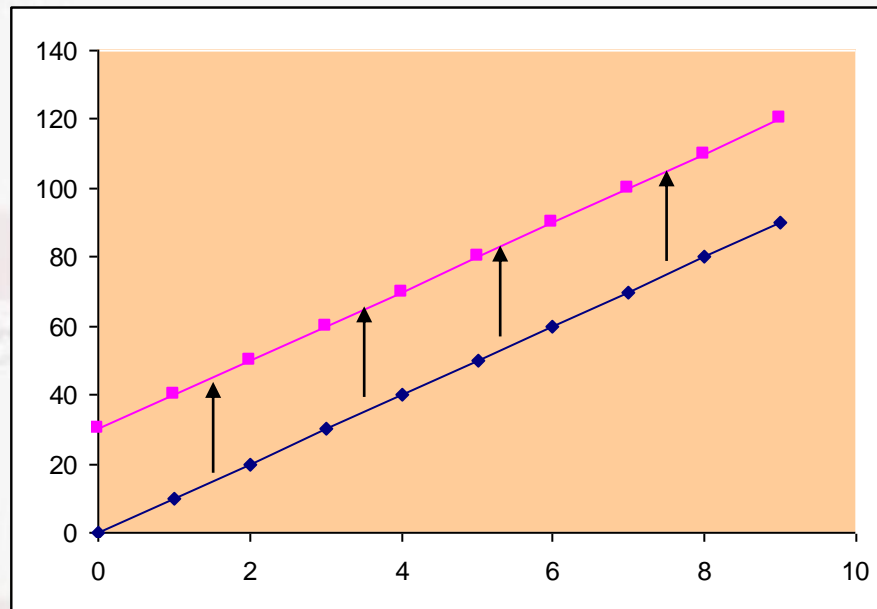
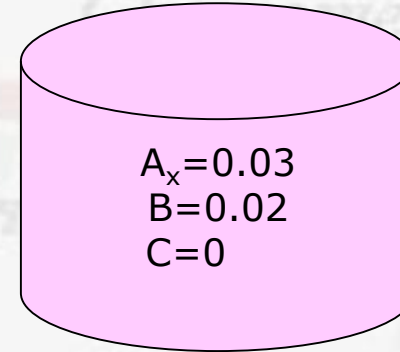
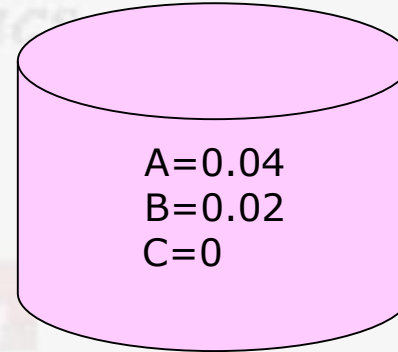
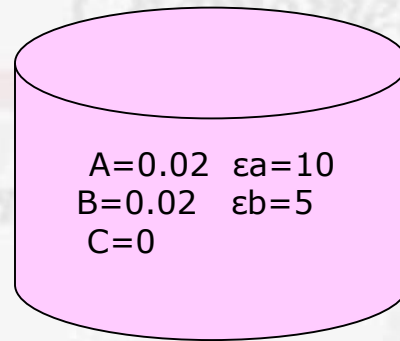
- spectral
- Non spectral

Blank spectral interference;

A=analyte

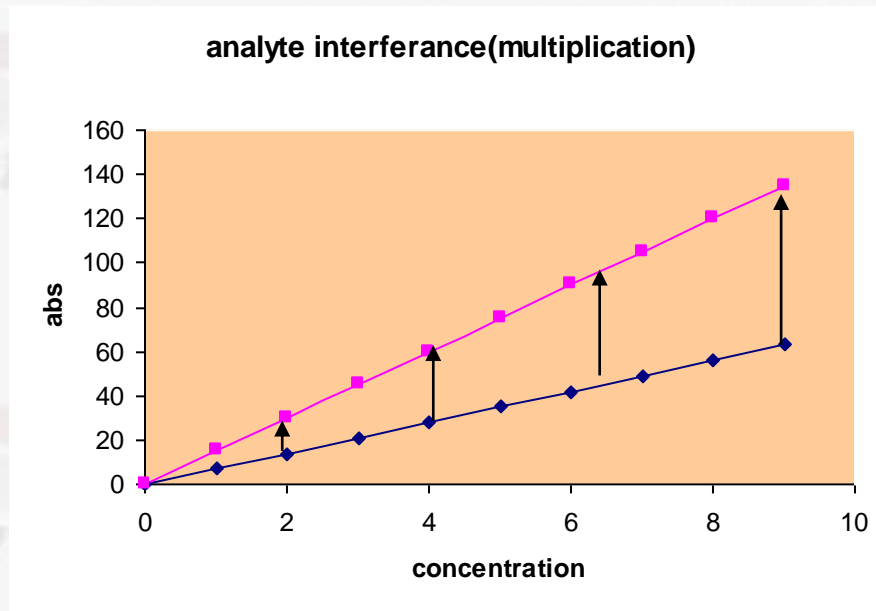
B=blank

C=interference



Additive interference

Analyte interference;



Non spectral analyte interference

Such as matrix effect cause error

Correspond to concentration of analyte.