# **Rheology of Fluids: Newtonian** to Non Newtonian

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## Instituet for advanced Studies in Basic Sciences May 2015

# Agenda:

- Fluid: Definition
- Rheology: Elementary concepts
- Navier-Stokes Equation
- Basic Solutions
- Dilute Suspension
- Non Newtonian
- OldRoyd Model

## Fluid:

Deborah number, a measure of fluidity

 $De = \frac{\tau_{relax}}{\tau_{exp}}$ Relaxation time in response to an externally applied force

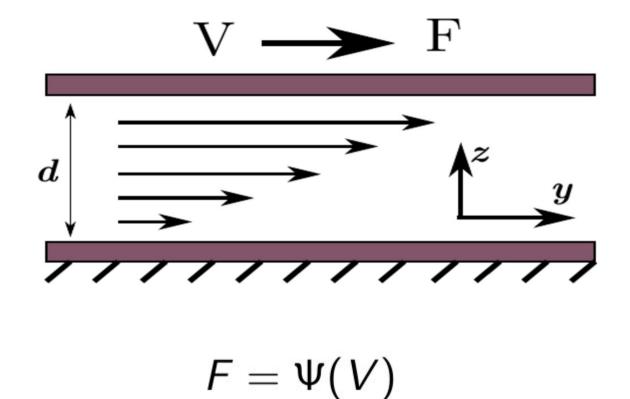




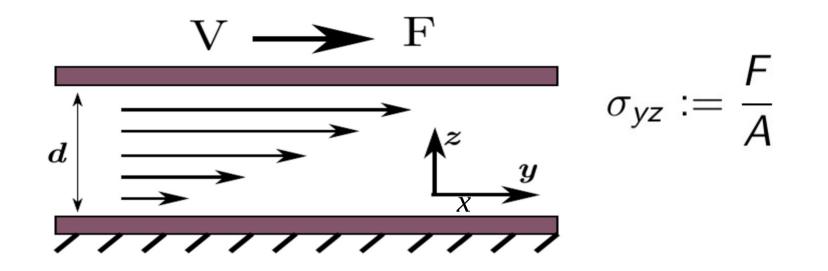


## **Rheology:**

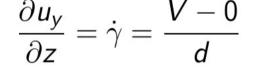
How does the system respond to an external force?



*Viscosity:* How does the system respond to an externally applied force?

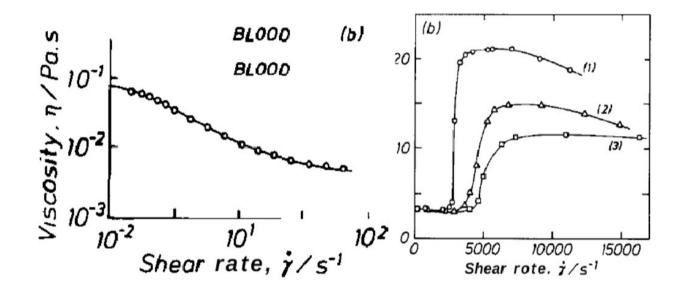


$$\sigma_{yz} = \Psi(\frac{\partial u_y}{\partial z})$$

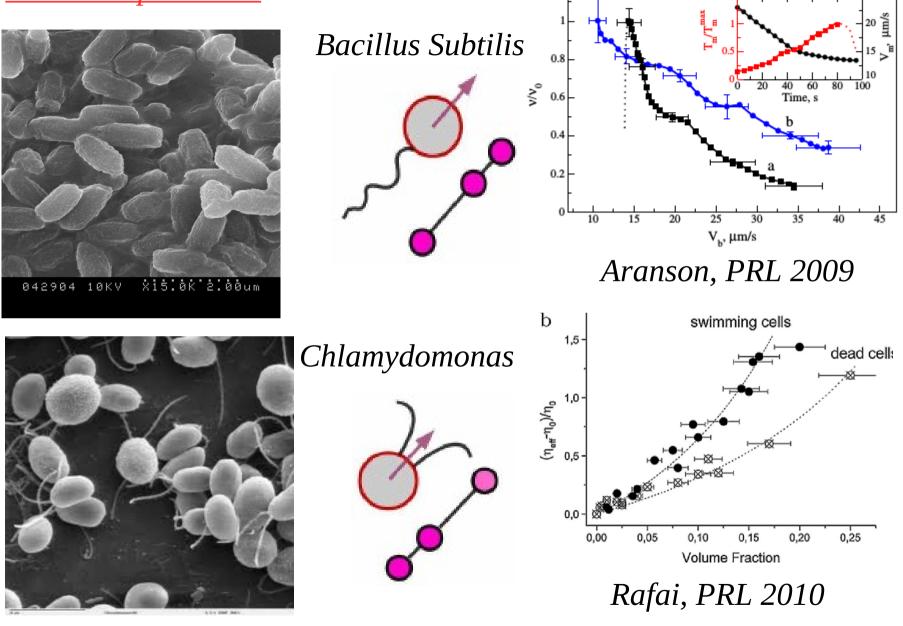


$$\sigma_{yz} = \eta \frac{\partial u_y}{\partial z} = \eta \dot{y}$$

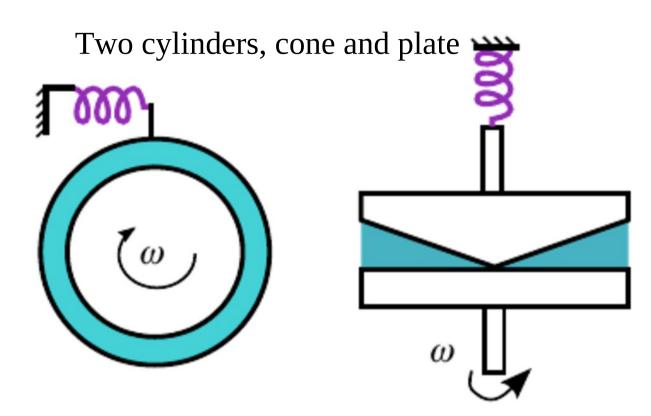
## 5/26 Some examples



#### 6/26 <u>Active Suspensions:</u>



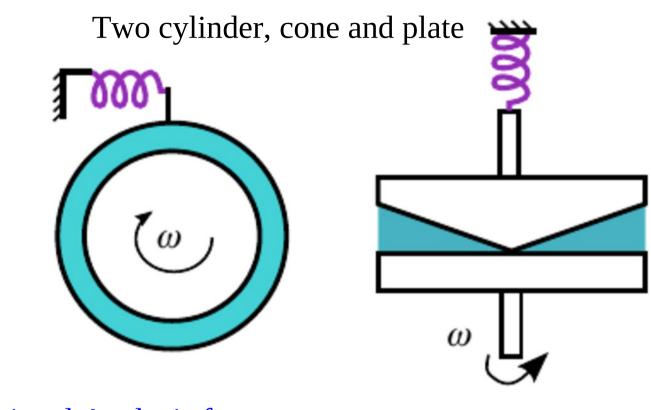
## 7/26 *Rheometry: Elementary tools*



Dimensional Analysis for water

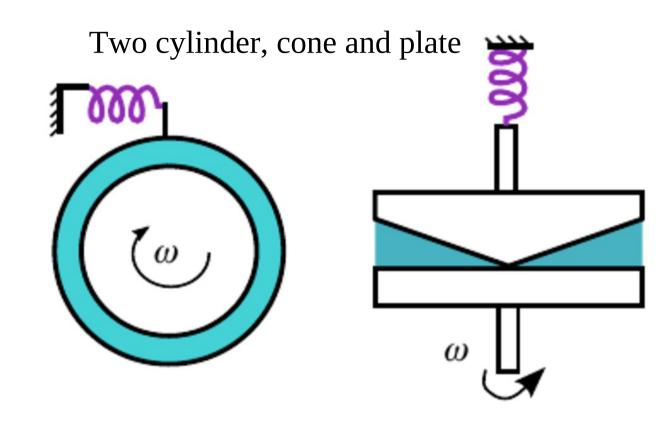
$$\eta \sim \frac{m}{lT}$$

## 7/26 *Rheometry: Elementary tools*



Dimensional Analysis for water  $\eta \sim \frac{m}{lT} \gamma e^{-\gamma \beta} kg$ 

## 7/26 *Rheometry: Elementary tools*

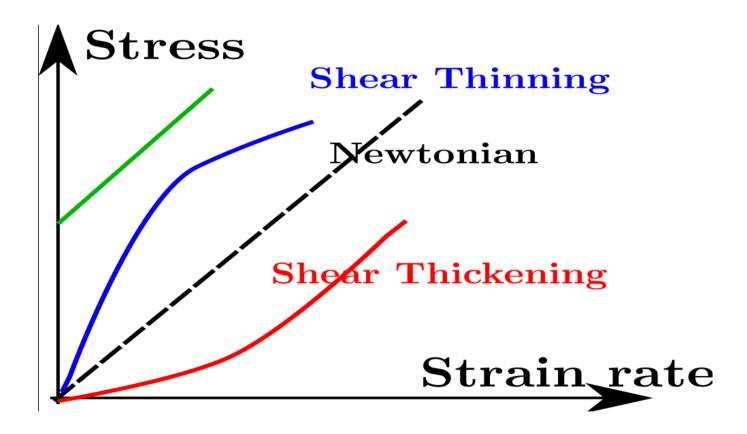


Dimensional Analysis for water  $\eta \sim \frac{m}{lT} \gamma \circ \frac{1}{2} kg$ 

 $\lambda \approx \mu m \longrightarrow \omega = c/\lambda \approx \nu^{\wedge}/\nu^{-\varphi} = \nu^{\nu}$  $T \approx \nu/\omega = \nu^{-\nu}s$ 

$$\eta \approx \frac{m}{l T} \approx 1 \circ^{-\tau} Pa.s$$

#### 8/26 Non-Newtonian



9/26 Toward the governing equations:

Velocity field  $\mathbf{u}(\mathbf{x}, t)$ 

Acceleration field

9/26 Toward the governing equations:

Velocity field 
$$\mathbf{u}(\mathbf{x}, t)$$

## Acceleration field

$$a(x,t) = (u(x+\delta x,t+\delta t) - u(x,t))/\delta t = i$$
$$\frac{d}{dt}u(x,t) = (\frac{\partial}{\partial t} + u \cdot \nabla)u(x,t)$$

9/26 Toward the governing equations:

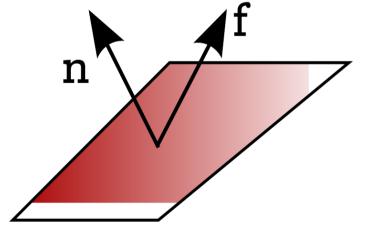
Velocity field 
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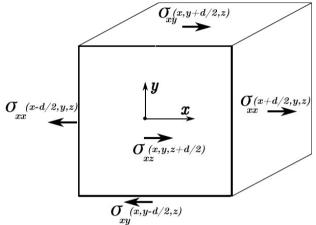
$$\sigma_{ij}(\mathbf{x}, t)$$
 Stress Tensor: i'th component of the the force exerted on a surface that is pointed to j direction

$$df_x = \sigma_{xx} ds_x + \sigma_{xy} ds_y + \sigma_{xz} ds_z$$
$$\mathbf{f} = \oint \boldsymbol{\sigma} \cdot d\mathbf{s}^T,$$



### 10/26 Governing equations

$$\mathbf{u}(\mathbf{x},t) = \sigma_{ij}(\mathbf{x},t)$$

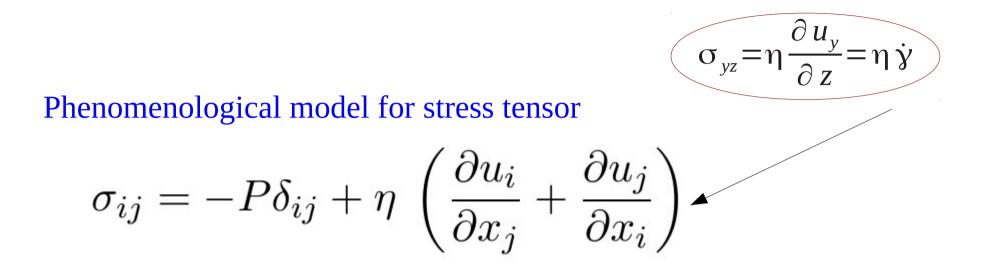


$$abla \cdot (
ho \mathbf{u}) + rac{\partial}{\partial t} 
ho = \circ \text{Continuity equation}$$

$$\rho(\mathbf{x},t) \times d\mathbf{v} \times \frac{d}{dt}\mathbf{u}(\mathbf{x},t) = \mathbf{F}(\mathbf{x},t) \times d\mathbf{v}$$

$$F_{x} = d^{\mathsf{T}} \times [\sigma_{xx}(x + \frac{d}{\mathsf{Y}}, y, z) - \sigma_{xx}(x - \frac{d}{\mathsf{Y}}, y, z) + \sigma_{xy}(x, y + \frac{d}{\mathsf{Y}}, z) - \sigma_{xx}(x, y, z) + \sigma_{xy}(x, y, z) + \sigma_{xy$$

#### 11/26 Governing Equations:



$$\frac{d}{dt}\mathbf{u}(\mathbf{x},t) = \left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \mathbf{u}(\mathbf{x},t)$$

## Hydrodynamics:

# Navier-Stokes Equation

$$ho\left(rac{\partial}{\partial t}+\mathbf{u}\cdot
abla
ight)\mathbf{u}(\mathbf{x},t)=\eta
abla^{2}\mathbf{u}(\mathbf{x},t)-
abla P(\mathbf{x},t),\qquad
abla\cdot\mathbf{u}=0$$

The Millennium Prize: 10<sup>6</sup>\$, The Clay Mathematics Institute of Cambridge, Massachusetts (CMI)

**Colloid's Universe: Low Reynolds Regime**:

$$\rho\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right)\mathbf{u} = -\nabla p + \eta \nabla^2 \mathbf{u}, \quad \nabla \cdot \mathbf{u} = 0$$

**Colloid's Universe: Low Reynolds Regime**:

$$\rho \left( \frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla \right) \mathbf{u} = -\nabla p + \eta \nabla^2 \mathbf{u}, \quad \nabla \cdot \mathbf{u} = 0$$
$$\mathcal{R}e = \frac{\left[ \rho(\mathbf{u} \cdot \nabla) \mathbf{u} \right]}{\eta \nabla^{\gamma} \mathbf{u}} \approx \frac{\rho V/L}{\eta/L^{\gamma}} = \frac{\rho VL}{\eta}$$

 $L=0.1 \mu m$ ,  $V=1 \mu m/S$ ,  $\eta=10^{-3} PaS$ ,  $\rho=10^{3} Kg/m^{3}$ 

 $Re \ll 1$ 

 $\eta \nabla^{\mathsf{T}} \mathbf{u}(\mathbf{x}) - \nabla P(\mathbf{x}) = \mathbf{f}(\mathbf{x}), \quad \nabla \mathbf{u}(\mathbf{x}) = \mathbf{0}$ 

## Hydrodynamics:

$$\eta \nabla^{\mathsf{r}} \mathbf{u}(\mathbf{x}) - \nabla P(\mathbf{x}) = \mathbf{f}(\mathbf{x}), \quad \nabla . \mathbf{u}(\mathbf{x}) = \circ$$

**Point force**:

$$\eta \nabla^{\mathsf{r}} \mathbf{u}(\mathbf{x}) - \nabla P(\mathbf{x}) = \mathbf{f}(\mathbf{x}), \quad \nabla . \mathbf{u}(\mathbf{x}) = \circ$$
**rce:**

$$\mathbf{f}(\mathbf{x}) = \mathbf{F}\delta(\mathbf{x})$$

$$u_{i}^{\circ}(\mathbf{x}) = \sum_{j} G_{ij}F_{j}, \quad G_{ij} = \frac{1}{\lambda \pi \eta r} \left(\delta_{ij} + \hat{r}_{i}\hat{r}_{j}\right)$$

## Hydrodynamics:

$$\eta \nabla^{\mathsf{T}} \mathbf{u}(\mathbf{x}) - \nabla P(\mathbf{x}) = \mathbf{f}(\mathbf{x}), \quad \nabla \cdot \mathbf{u}(\mathbf{x}) = \circ$$

**Point force**:

$$\eta \nabla^{\gamma} \mathbf{u}(\mathbf{x}) - \nabla P(\mathbf{x}) = \mathbf{f}(\mathbf{x}), \quad \nabla . \mathbf{u}(\mathbf{x}) = \circ$$
F
$$\mathbf{f}(\mathbf{x}) = \mathbf{F}\delta(\mathbf{x})$$

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Force Dipole:

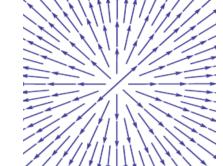
$$\mathbf{u}^D = (\mathbf{G}(\mathbf{x} + \mathbf{d}) - \mathbf{G}(\mathbf{x})) \cdot \mathbf{F}$$

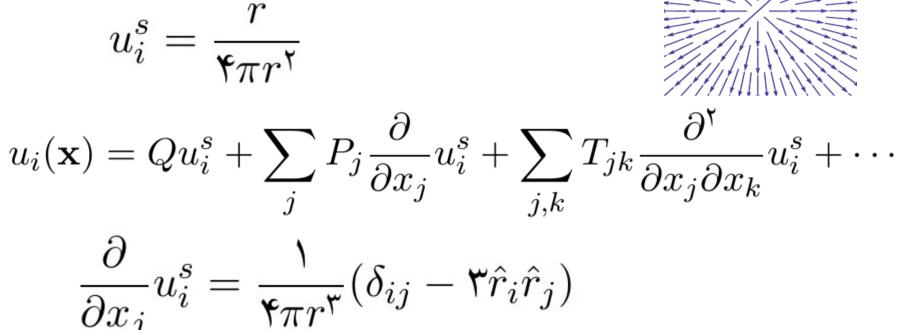
$$u_{i}^{D} = \sum_{j,k} G_{ijk}^{D} P_{kj} \qquad P_{kj} = d_{k}F_{j}$$
$$G_{ijk}^{D} = \frac{\partial}{\partial x_{k}} G_{ij} = \frac{1}{\lambda \pi \eta r^{\dagger}} \left( \delta_{ij} \hat{r}_{k} - \delta_{ik} \hat{r}_{j} + \delta_{jk} \hat{r}_{i} + \mathbf{\tilde{r}} \hat{r}_{i} \hat{r}_{j} \hat{r}_{k} \right)$$

## **Multipole Expansion:**

$$\begin{split} u_{i}(\mathbf{x}) &= \sum_{j} G_{ij}b_{j} + \sum_{j,k} G_{ijk}^{D}p_{jk} \\ &+ \sum_{j,k,l} G_{ijkl}^{Q}t_{jkl} + j_{kl} + j_{kl} \\ G_{ij} &= \frac{1}{\lambda \pi \eta r} \left( \delta_{ij} + \hat{r}_{i}\hat{r}_{j} \right) \\ G_{ijk}^{D} &= \frac{\partial}{\partial x_{k}} G_{ij} \\ G_{ijlm}^{Q} &= \frac{\partial}{\partial x_{m}} G_{ijl}^{D} \end{split}$$

#### Sink and Source another singular solutions:

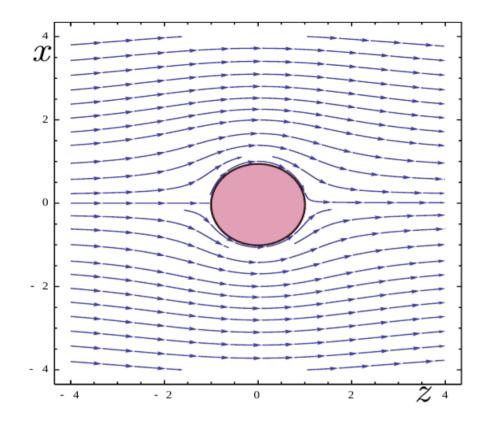




# Moving Sphere:

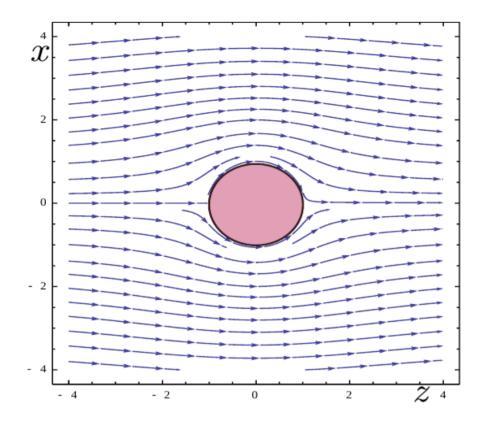
$$u_i(\mathbf{x}) = \sum_j \left( b_j G_{ij} + P_j \frac{\partial}{\partial x_j} u_i^s \right)$$

$$|\mathbf{u}(\mathbf{x})|_{\mathbf{x}=R} = \mathbf{V}_{\circ}$$



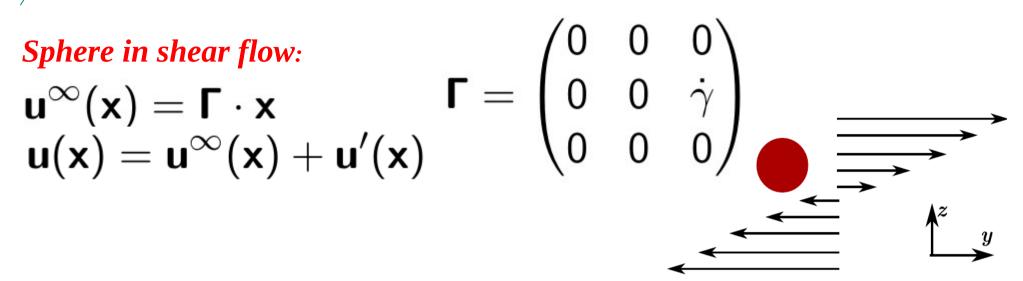
# Moving Sphere:

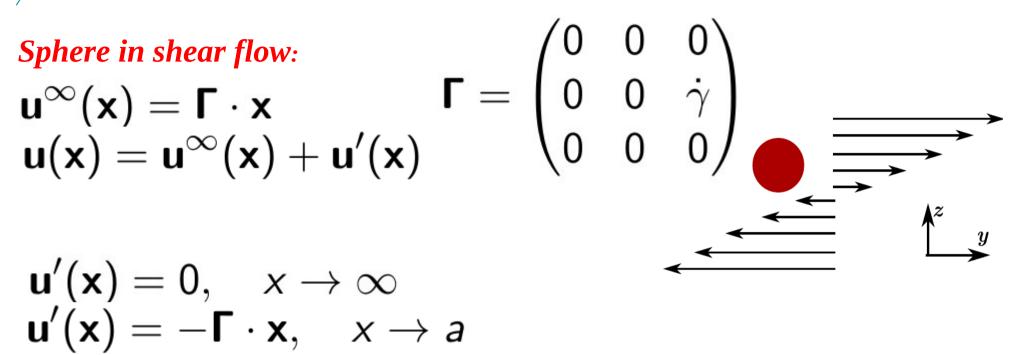
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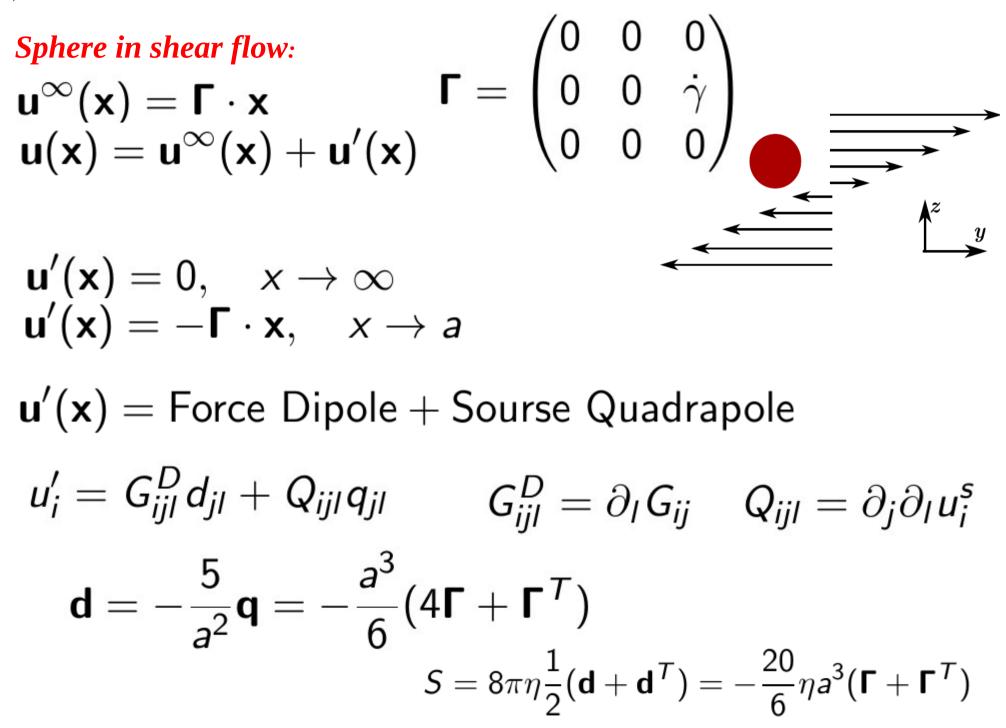
$$\mathbf{P} = \pi R^{\mathsf{r}} \mathbf{V}_{\circ}, \quad \mathbf{b} = \mathbf{\mathcal{P}} \pi \eta R \mathbf{V}_{\circ}$$

$$\mathbf{u}(\mathbf{r}) = \left(\frac{\mathbf{\tilde{r}}}{\mathbf{\tilde{r}}}(\frac{R}{r})(I+\hat{r}\hat{r}) + \frac{\mathbf{\tilde{r}}}{\mathbf{\tilde{r}}}(\frac{R}{r})^{\mathbf{\tilde{r}}}(I-\mathbf{\tilde{r}}\hat{r})\right) \cdot \mathbf{V}$$



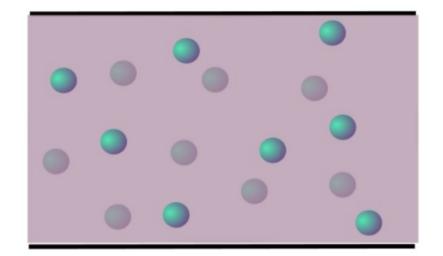


 $\mathbf{u}'(\mathbf{x}) = Force Dipole + Sourse Quadrapole$ 



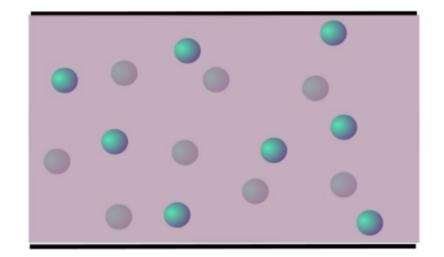
#### **Passive suspension:** Einstein's theory

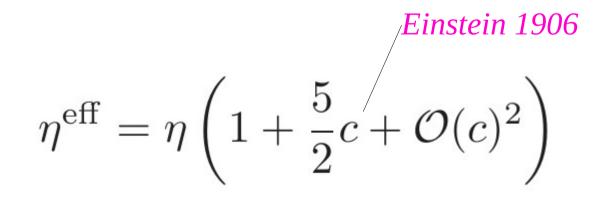
 $\eta^{\text{eff}} \sim \frac{\Sigma}{\nabla \mathbf{u}}$  ?



#### **Passive suspension:** Einstein's theory

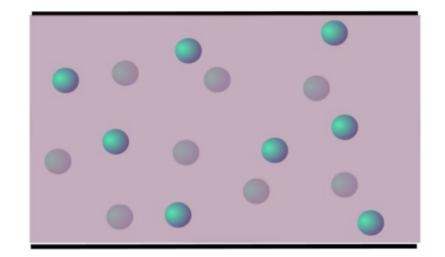
 $\eta^{\text{eff}} \sim \frac{\Sigma}{\nabla \mathbf{u}}$  ?

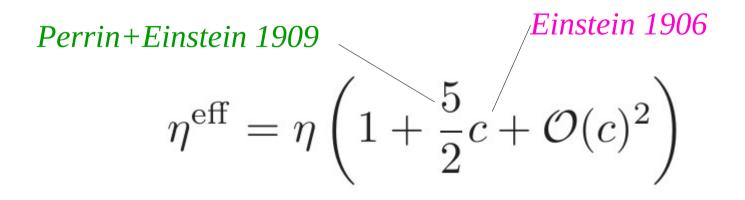




#### **Passive suspension:** Einstein's theory

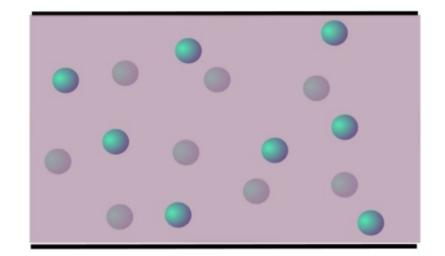
 $\eta^{\rm eff} \sim \frac{\Sigma}{\nabla \mathbf{u}}$  ?

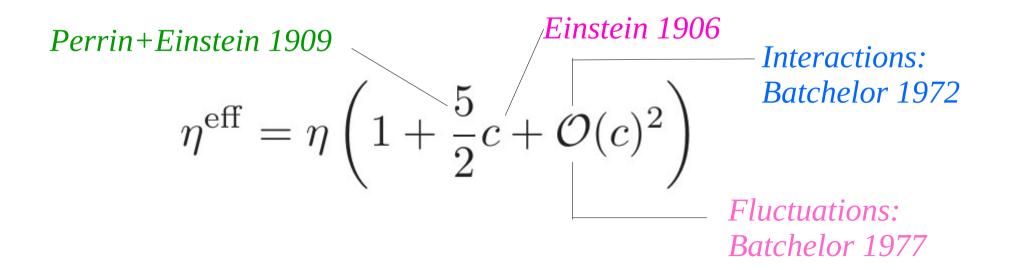




#### **Passive suspension:** Einstein's theory

 $\eta^{\text{eff}} \sim \frac{\Sigma}{\nabla \mathbf{u}}$  ?





$$\sigma_{ij} = -P\delta_{ij} + \eta \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i}\right) \qquad \mathbf{V}$$
$$\mathbf{S}_{\mathbf{S}_{\mathbf{O}}}^{\mathbf{V}_{\mathbf{O}}}$$
$$\langle \sigma_{ij} \rangle = \frac{1}{V} \int_{V} \sigma_{ij} d\mathbf{v} = \frac{1}{V} \int_{V-V_0} \sigma_{ij} d\mathbf{v} + \frac{1}{V} \int_{V_0} \sigma_{ij} d\mathbf{v}$$

$$\begin{aligned}
\pi ij &= -P\delta_{ij} + \eta \left( \frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) & \mathsf{V} \\
\mathbf{s}_0^{\mathsf{V}_0} \\
\langle \sigma_{ij} \rangle &= \frac{1}{V} \int_V \sigma_{ij} d\mathsf{v} = \frac{1}{V} \int_{V-V_0} \sigma_{ij} d\mathsf{v} + \frac{1}{V} \int_{V_0} \sigma_{ij} d\mathsf{v} \\
& \int_V \partial_k (\sigma_{kj} x_i) = \int_V (\partial_k \sigma_{kj}) x_i + \int_V \sigma_{kj} \delta_{ki} \\
& \oint_S \sigma_{kj} x_i n_k = 0 + \int_V \sigma_{ij} \\
& = \frac{1}{V} \int_{V-V_0} \sigma_{ij} d\mathsf{v} + \frac{1}{V} \int_{S_0} x_i \sigma_{jk} n_k ds
\end{aligned}$$

$$19/26$$

$$\sigma_{ij} = -P\delta_{ij} + \eta \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i}\right) \quad \mathbf{V}$$

$$\mathbf{S}_{0}^{\mathbf{V}_{0}}$$

$$\langle \sigma_{ij} \rangle = \frac{1}{V} \int_{V} \sigma_{ij} d\mathbf{v} = \frac{1}{V} \int_{V-V_0} \sigma_{ij} d\mathbf{v} + \frac{1}{V} \int_{V_0} \sigma_{ij} d\mathbf{v}$$

$$\int_{V} \partial_k (\sigma_{kj} x_i) = \int_{V} (\partial_k \sigma_{kj}) x_i + \int_{V} \sigma_{kj} \delta_{ki}$$

$$\oint_{S} \sigma_{kj} x_i n_k = 0 + \int_{V} \sigma_{ij}$$

$$= \frac{1}{V} \int_{V-V_0} \sigma_{ij} d\mathbf{v} + \frac{1}{V} \int_{S_0} x_i \sigma_{jk} n_k ds$$

$$= \frac{1}{V} \int_{V-V_0} (-P\delta_{ij} + \eta(\partial_i u_j + \partial_j u_i)) d\mathbf{v} + \frac{1}{V} \int_{S_0} x_i f_j ds \quad f_i = \sigma_{jk} n_k$$

$$19/26$$

$$\sigma_{ij} = -P\delta_{ij} + \eta \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i}\right) \quad \forall \quad s_0^{(V)}$$

$$\langle \sigma_{ij} \rangle = \frac{1}{V} \int_V \sigma_{ij} dv = \frac{1}{V} \int_{V-V_0} \sigma_{ij} dv + \frac{1}{V} \int_{V_0} \sigma_{ij} dv$$

$$\int_V \partial_k (\sigma_{kj} x_i) = \int_V (\partial_k \sigma_{kj}) x_i + \int_V \sigma_{kj} \delta_{ki}$$

$$\int_S \sigma_{kj} x_i n_k = 0 + \int_V \sigma_{ij}$$

$$= \frac{1}{V} \int_{V-V_0} \sigma_{ij} dv + \frac{1}{V} \int_{S_0} x_i \sigma_{jk} n_k ds$$

$$= \frac{1}{V} \int_{V-V_0} (-P\delta_{ij} + \eta(\partial_i u_j + \partial_j u_i)) dv + \frac{1}{V} \int_{S_0} x_i f_j ds \quad f_i = \sigma_{ik} n_k$$

$$= \frac{1}{V} \delta_{ij} \int_{V-V_0} P dv + \eta \langle (\partial_i u_j + \partial_j u_i) \rangle + \frac{1}{V} \int_{S_0} (x_i f_j - \eta(u_i n_j + u_j n_i)) ds$$

$$= \frac{1}{V} \delta_{ij} \int_{V-V_0} P dv + \eta \langle (\partial_i u_j + \partial_j u_i) \rangle + \frac{1}{V} S_{ij}$$
Force Dipole

Simple shear flow

$$\mathbf{u}(\mathbf{x}) = \mathbf{\Gamma} \cdot \mathbf{x}$$
  
$$\eta \langle (\partial_i u_j + \partial_j u_i) \rangle + \frac{1}{V} S_{ij} = \eta (\mathbf{\Gamma} + \mathbf{\Gamma}^T) + 0$$

Simple shear flow

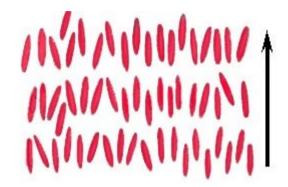
$$\mathbf{u}(\mathbf{x}) = \mathbf{\Gamma} \cdot \mathbf{x}$$
  
$$\eta \langle (\partial_i u_j + \partial_j u_i) \rangle + \frac{1}{V} S_{ij} = \eta (\mathbf{\Gamma} + \mathbf{\Gamma}^T) + 0$$

# Simple shear flow + Sphere $\eta \langle (\partial_i u_j + \partial_j u_i) \rangle + \frac{1}{V} S_{ij} = \eta (\mathbf{\Gamma} + \mathbf{\Gamma}^T) + \frac{1}{V} \frac{20\pi}{6} \eta a^3 (\mathbf{\Gamma} + \mathbf{\Gamma}^T)$ $\eta \to (1 + 5/2\phi)\eta$ $\phi = N(\frac{4}{3}\pi a^3)/(V)$

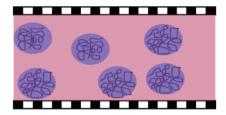
21/26 Non Newtonian Behavior:

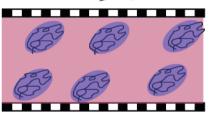
Microscopic anisotropy

I: Intrinsic → Liquid Crystal



II: Induced anisotropy  $\rightarrow$  Polymeric solutions

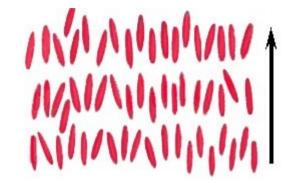


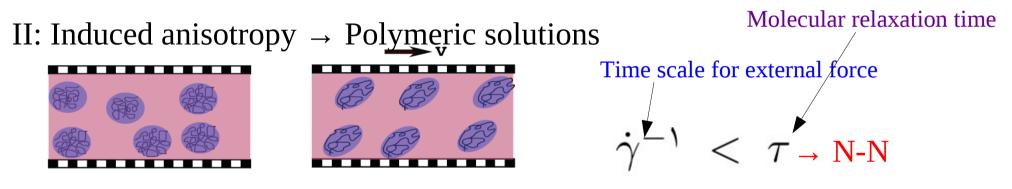


21/26 Non Newtonian Behavior:

Microscopic anisotropy

I: Intrinsic → Liquid Crystal





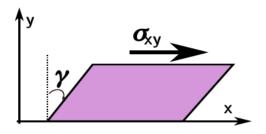
Molecules will not have enough time to response and reach their isotropic structure

Relaxation time for water= $1 \circ - 17 s$ 

We expect to see N-N behavior in water for frequencies >\  $\circ$  `` Hz

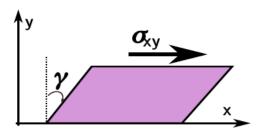
$$\sigma_{xy} = \eta(\dot{\gamma})\dot{\gamma}, \qquad \sigma_{xz} = \sigma_{zy} = \circ,$$

$$\sigma_{xx} \quad - \quad \sigma_{yy} = N_{\rm I}(\dot{\gamma}), \qquad \sigma_{yy} - \sigma_{zz} = N_{\rm I}(\dot{\gamma})$$

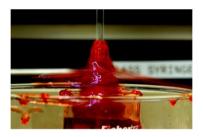


$$\sigma_{xy} = \eta(\dot{\gamma})\dot{\gamma}, \qquad \sigma_{xz} = \sigma_{zy} = \circ,$$

$$\sigma_{xx} \quad - \quad \sigma_{yy} = N_{\mathsf{T}}(\dot{\gamma}), \qquad \sigma_{yy} - \sigma_{zz} = N_{\mathsf{T}}(\dot{\gamma})$$

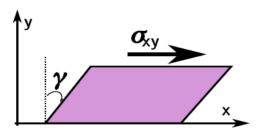


Normal Stress Differences Macroscopic Manifestation: Weisenberg Effect

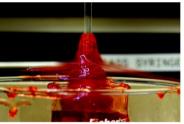


$$\sigma_{xy} = \eta(\dot{\gamma})\dot{\gamma}, \qquad \sigma_{xz} = \sigma_{zy} = \circ$$

$$\sigma_{xx} - \sigma_{yy} = N_{\mathrm{T}}(\dot{\gamma}), \quad \sigma_{yy} - \sigma_{zz} = N_{\mathrm{T}}(\dot{\gamma})$$



Normal Stress Differences Macroscopic Manifestation: Weisenberg Effect



Shear thickening: Viscosity increases by increasing external shear برش وشكسان: نشاسته ذرت و آب

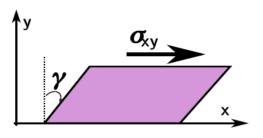
<mark>Shear thinning</mark>: Viscosity decreases by increasing external shear برش روان: سس گوجه



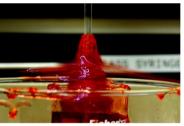


$$\sigma_{xy} = \eta(\dot{\gamma})\dot{\gamma}, \qquad \sigma_{xz} = \sigma_{zy} = \circ,$$

$$\sigma_{xx} - \sigma_{yy} = N_{\mathrm{T}}(\dot{\gamma}), \quad \sigma_{yy} - \sigma_{zz} = N_{\mathrm{T}}(\dot{\gamma})$$



Normal Stress Differences Macroscopic Manifestation: Weisenberg Effect



Shear thickening: Viscosity increases by increasing external shear برش وشكسان: نشاسته ذرت و آب

<mark>Shear thinning</mark>: Viscosity decreases by increasing external shear برش روان: سس گوجه

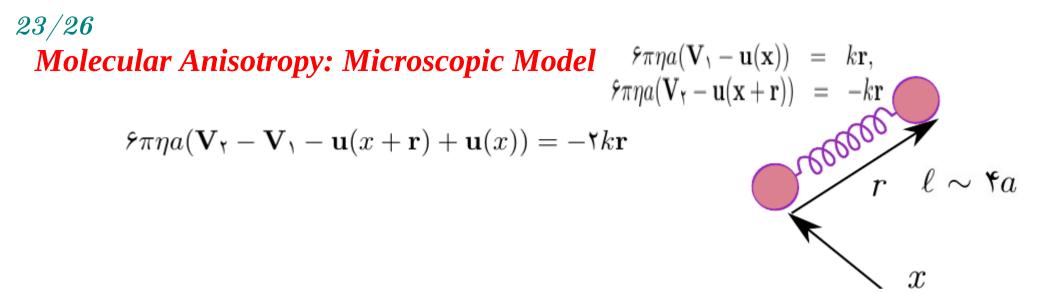




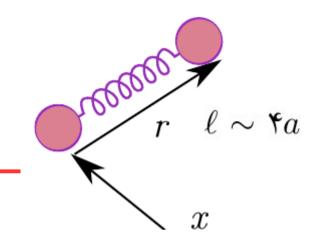
Viscoelastic Behavior → Kelvin Voigt Model

$$\sigma = G\gamma + \eta \dot{\gamma}$$
$$\gamma(t) = \gamma_{\circ} e^{-i\omega t}$$

 $\sigma(t) = G(\omega)\gamma(t)$   $\tilde{G}(\omega) = G - i\omega\eta$ 



$$\begin{aligned} & \Im \pi \eta a (\mathbf{V}_{\mathsf{T}} - \mathbf{V}_{\mathsf{T}} - \mathbf{u}(x + \mathbf{r}) + \mathbf{u}(x)) = -\mathsf{T}k\mathbf{r} \\ & \Im \pi \eta a \frac{d}{dt}\mathbf{r} = -\mathsf{T}k\mathbf{r} + \Im \pi \eta a(\mathbf{r} \cdot \nabla)\mathbf{u}(\mathbf{x}) \end{aligned}$$



$$\begin{aligned} & \Im \pi \eta a (\mathbf{V}_{\mathsf{T}} - \mathbf{V}_{\mathsf{T}} - \mathbf{u}(x + \mathbf{r}) + \mathbf{u}(x)) = -\mathsf{T}k\mathbf{r} \\ & \Im \pi \eta a \frac{d}{dt}\mathbf{r} = -\mathsf{T}k\mathbf{r} + \Im \pi \eta a(\mathbf{r} \cdot \nabla)\mathbf{u}(\mathbf{x}) \end{aligned}$$

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$$\begin{aligned} \frac{d}{dt}\mathbf{r} &= -\frac{1}{\mathbf{r}\tau}\mathbf{r} + (\mathbf{r}\cdot\nabla)\mathbf{u}(\mathbf{x}) + (\frac{1}{\mathbf{r}\pi\eta a})\mathbf{f}(t) \\ \langle f_i(t)f_j(t')\rangle &= \mathbf{r}\xi k_B T \delta_{ij}\delta(t-t') \end{aligned} \qquad \tau &= \mathbf{r}\pi\eta a/\mathbf{r}k \end{aligned}$$

$$\begin{split} & \frac{\Im \pi \eta a (\mathbf{V}_{\mathbf{Y}} - \mathbf{V}_{\mathbf{Y}} - \mathbf{u}(x + \mathbf{r}) + \mathbf{u}(x)) = -\mathbf{Y} k \mathbf{r}}{\Im \pi \eta a \frac{d}{dt} \mathbf{r}} = -\mathbf{Y} k \mathbf{r} + \Im \pi \eta a (\mathbf{r} \cdot \nabla) \mathbf{u}(\mathbf{x}) \\ & \frac{d}{dt} \mathbf{r} = -\frac{\mathbf{Y}}{\mathbf{Y} \tau} \mathbf{r} + (\mathbf{r} \cdot \nabla) \mathbf{u}(\mathbf{x}) + (\frac{\mathbf{Y}}{\Im \pi \eta a}) \mathbf{f}(t) \\ & \frac{d}{f_i(t) f_j(t')} = \mathbf{Y} \xi k_B T \delta_{ij} \delta(t - t') \end{split}$$

$$\sigma^P \cdot d\mathbf{s} = (k\mathbf{r})(\mathcal{N}\mathbf{r} \cdot d\mathbf{s}) \qquad \sigma^P = \mathcal{N}k\mathbf{r}\mathbf{r} \qquad \mathbf{r} = \mathbf{r}(\mathbf{x}, t)$$

$$\sigma^P \cdot d\mathbf{s} = (k\mathbf{r})(\mathcal{N}\mathbf{r} \cdot d\mathbf{s}) \qquad \sigma^P = \mathcal{N}k\mathbf{r}\mathbf{r} \qquad \mathbf{r} = \mathbf{r}(\mathbf{x}, t)$$

$$\begin{split} & \frac{\Im \pi \eta a (\mathbf{V}_{\mathbf{Y}} - \mathbf{V}_{\mathbf{Y}} - \mathbf{u}(x + \mathbf{r}) + \mathbf{u}(x)) = -\mathbf{V} k \mathbf{r}}{\Im \pi \eta a \frac{d}{dt} \mathbf{r}} = -\mathbf{V} k \mathbf{r} + \Im \pi \eta a (\mathbf{r} \cdot \nabla) \mathbf{u}(\mathbf{x}) & \mathbf{v} \\ & \frac{d}{dt} \mathbf{r} = -\frac{\mathbf{V}}{\mathbf{V} \tau} \mathbf{r} + (\mathbf{r} \cdot \nabla) \mathbf{u}(\mathbf{x}) + (\frac{\mathbf{V}}{\Im \pi \eta a}) \mathbf{f}(t) \\ & \frac{d}{f_i(t) f_j(t')} = \mathbf{V} \xi k_B T \delta_{ij} \delta(t - t') & \tau = \Im \pi \eta a / \mathbf{V} k \end{split}$$

$$\sigma^P \cdot d\mathbf{s} = (k\mathbf{r})(\mathcal{N}\mathbf{r} \cdot d\mathbf{s}) \qquad \sigma^P = \mathcal{N}k\mathbf{r}\mathbf{r} \qquad \mathbf{r} = \mathbf{r}(\mathbf{x}, t)$$

$$\begin{split} & \frac{\Im \pi \eta a (\mathbf{V}_{\mathbf{Y}} - \mathbf{V}_{\mathbf{Y}} - \mathbf{u}(x + \mathbf{r}) + \mathbf{u}(x)) = -\mathbf{Y} k \mathbf{r} \\ & \frac{\Im \pi \eta a \frac{d}{dt} \mathbf{r} = -\mathbf{Y} k \mathbf{r} + \Im \pi \eta a (\mathbf{r} \cdot \nabla) \mathbf{u}(\mathbf{x}) \\ & \frac{d}{dt} \mathbf{r} = -\frac{\mathbf{Y}}{\mathbf{Y} \tau} \mathbf{r} + (\mathbf{r} \cdot \nabla) \mathbf{u}(\mathbf{x}) + (\frac{\mathbf{Y}}{\Im \pi \eta a}) \mathbf{f}(t) \\ & \frac{\chi}{\langle f_i(t) f_j(t') \rangle} = \mathbf{Y} \xi k_B T \delta_{ij} \delta(t - t') \end{split}$$

$$\sigma^P \cdot d\mathbf{s} = (k\mathbf{r})(\mathcal{N}\mathbf{r} \cdot d\mathbf{s}) \qquad \sigma^P = \mathcal{N}k\mathbf{r}\mathbf{r} \qquad \mathbf{r} = \mathbf{r}(\mathbf{x}, t)$$

After averaging over noise, it is easy to show:  $\boldsymbol{\Sigma} = \frac{\boldsymbol{\gamma}}{\mathcal{N}k_BT}\sigma^P$  $\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \boldsymbol{\Sigma} - \boldsymbol{\Sigma} \cdot \nabla \mathbf{u} - \nabla \mathbf{u}^T \cdot \boldsymbol{\Sigma} = -\frac{\boldsymbol{\gamma}}{\tau} \left(\boldsymbol{\Sigma} - I\right)$ 

24/26  
OldRoyd Model 
$$\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \mathbf{u} = \nabla \cdot \sigma, \quad \nabla \cdot \mathbf{u} = \circ,$$
  
 $\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \mathbf{\Sigma} - \mathbf{\Sigma} \cdot \nabla \mathbf{u} - \nabla \mathbf{u}^T \cdot \mathbf{\Sigma} = -\frac{1}{\tau} (\mathbf{\Sigma} - I)$   
 $\sigma = -PI + \eta (\nabla \mathbf{u} + \nabla \mathbf{u}^T) + g\mathbf{\Sigma} \quad g = \frac{1}{\tau} \mathcal{N} k_B T$ 

24/26  
OldRoyd Model 
$$\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \mathbf{u} = \nabla \cdot \sigma, \quad \nabla \cdot \mathbf{u} = \circ,$$
  
 $\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \mathbf{\Sigma} - \mathbf{\Sigma} \cdot \nabla \mathbf{u} - \nabla \mathbf{u}^T \cdot \mathbf{\Sigma} = -\frac{\lambda}{\tau} (\mathbf{\Sigma} - I)$   
 $\sigma = -PI + \eta (\nabla \mathbf{u} + \nabla \mathbf{u}^T) + g\mathbf{\Sigma} \quad g = \frac{\lambda}{\tau} \mathcal{N} k_B T$   
Response to a simple shear flow:

$$\mathbf{u} = (\dot{\gamma}y, \circ, \circ) \qquad \nabla \mathbf{u} = \begin{pmatrix} \circ & \circ \\ \dot{\gamma} & \circ \end{pmatrix} \qquad \mathbf{\Sigma} = \begin{pmatrix} \Sigma_{xx} & \Sigma_{xy} \\ \Sigma_{xy} & \Sigma_{yy} \end{pmatrix}$$

24/26  
OldRoyd Model 
$$\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \mathbf{u} = \nabla \cdot \sigma, \quad \nabla \cdot \mathbf{u} = \circ,$$
  
 $\left(\frac{\partial}{\partial t} + \mathbf{u} \cdot \nabla\right) \mathbf{\Sigma} - \mathbf{\Sigma} \cdot \nabla \mathbf{u} - \nabla \mathbf{u}^T \cdot \mathbf{\Sigma} = -\frac{1}{\tau} (\mathbf{\Sigma} - I)$   
 $\sigma = -PI + \eta (\nabla \mathbf{u} + \nabla \mathbf{u}^T) + g\mathbf{\Sigma} \quad g = \frac{1}{\tau} \mathcal{N} k_B T$ 

Response to a simple shear flow:

$$\mathbf{u} = (\dot{\gamma}y, \circ, \circ) \qquad \nabla \mathbf{u} = \begin{pmatrix} \circ & \circ \\ \dot{\gamma} & \circ \end{pmatrix} \qquad \mathbf{\Sigma} = \begin{pmatrix} \Sigma_{xx} & \Sigma_{xy} \\ \Sigma_{xy} & \Sigma_{yy} \end{pmatrix}$$
$$\dot{\gamma} \begin{pmatrix} \Upsilon \Sigma_{xy} & \Sigma_{yy} \\ \Sigma_{yy} & \circ \end{pmatrix} = \frac{1}{\tau} \begin{pmatrix} \Sigma_{xx} - 1 & \Sigma_{xy} \\ \Sigma_{xy} & \Sigma_{yy} - 1 \end{pmatrix}$$

$$\begin{array}{l} 24/26\\ OldRoyd\ Model\ \left(\frac{\partial}{\partial t}+\mathbf{u}\cdot\nabla\right)\mathbf{u}=\nabla\cdot\sigma,\quad\nabla\cdot\mathbf{u}=\circ,\\ \left(\frac{\partial}{\partial t}+\mathbf{u}\cdot\nabla\right)\boldsymbol{\Sigma}-\boldsymbol{\Sigma}\cdot\nabla\mathbf{u}-\nabla\mathbf{u}^{T}\cdot\boldsymbol{\Sigma}=-\frac{1}{\tau}\left(\boldsymbol{\Sigma}-I\right)\\ \sigma=-PI+\eta(\nabla\mathbf{u}+\nabla\mathbf{u}^{T})+g\boldsymbol{\Sigma}\quad g=\frac{1}{\tau}\mathcal{N}k_{B}T\\ \hline \mathbf{Response\ to\ a\ simple\ shear\ flow:}\\ \mathbf{u}=\left(\dot{\gamma}y,\circ,\circ\right)\quad\nabla\mathbf{u}=\left(\begin{array}{c}\circ&\circ\\\dot{\gamma}&\circ\end{array}\right)\quad\boldsymbol{\Sigma}=\left(\begin{array}{c}\Sigma_{xx}\quad\Sigma_{xy}\\\Sigma_{xy}\quad\Sigma_{yy}\end{array}\right)\\ \dot{\gamma}\left(\begin{array}{c}\Upsilon\Sigma_{xy}\quad\Sigma_{yy}\\\Sigma_{yy}&\circ\end{array}\right)=\frac{1}{\tau}\left(\begin{array}{c}\Sigma_{xx}-1\quad\Sigma_{xy}\\\Sigma_{xy}\quad\Sigma_{yy}-1\end{array}\right)\\ \Sigma_{xx}=1+\Upsilon\dot{\gamma}^{\dagger}\tau^{\intercal},\quad\Sigma_{xy}=\dot{\gamma}\tau,\quad\Sigma_{yy}=1\\ \sigma=\left(\begin{array}{c}-P&\eta\dot{\gamma}\\\eta\dot{\gamma}&-P\end{array}\right)+g\left(\begin{array}{c}1+\Upsilon\dot{\gamma}^{\dagger}\tau^{\intercal}&\dot{\gamma}\tau\\\dot{\gamma}\tau&1\end{array}\right)\quad \begin{array}{c}N_{1}=\sigma_{xx}-\sigma_{yy}=\Upsilon g\dot{\gamma}^{\intercal}\tau^{\intercal}\\ \eta_{e}=\eta+g\tau=\eta(1+\epsilon)\end{array}$$

 $\epsilon = (\mathbf{r}/\mathbf{f})\pi \mathcal{N}k_B T a/k$ 

Response to an harmonic shear flow:

$$\mathbf{u} = (\dot{\gamma}y, \circ, \circ)$$
$$\dot{\gamma}(t) = a\omega \cos \omega t$$

$$\sigma_{xy} = \tilde{G}(\omega)\gamma(t)$$
$$\tilde{G}(\omega) = G_r(\omega) + iG_i(\omega)$$

$$G_r(\omega) = ?$$
  
 $G_i(\omega) = ?$ 

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